

Method Comparison of the Evaluation of the Cylindricity Deviation Measured by Different Measurement Strategies

Miroslav Dovica^{1*}, Ján Buša²

¹ Department of Biomedical Engineering and Measurement, Faculty of Mechanical Engineering, Letná 9, 04200 Košice, Slovak Republic

² Department of Mathematics and Theoretical Informatics, Faculty of Electrical Engineering and Informatics, Technical University of Košice, Némcevej 32, 040 01 Košice, Slovak Republic

BIOGRAPHICAL NOTES

Miroslav Dovica is a professor of metrology and a deputy head of the Department of Biomedical Engineering and Measurement. He has published 2 monographs, 2 university text books, 4 university notebooks and more than 160 publications in journals and conference proceedings in Slovakia and abroad. He raised a Laboratory of Coordinate Metrology for the Department of Biomedical Engineering and Measurement.

Ján Buša was born on 30. 6. 1958. In 1982, he graduated (RNDr) with distinction at the Department of Computational Physics at the Faculty of Numerical Mathematics and Cybernetics in Moscow State University in Russia. He defended his CSc in the field of Applied Mathematics in 1987; his thesis title was "Solving the Linear Systems with Inaccurate Given Data". Since 1986, he has been working as a teacher at the Department of Mathematics and Theoretical Informatics. His scientific research focuses on applied mathematics and numerical methods.

KEY WORDS

Cylindricity deviation, measurement strategy, linear least squares method (LLS), coordinate measuring machine (CMM)..

ABSTRACT

The aim of this paper is to compare the quantitative parameters of methods used for the evaluation of the cylindricity deviation. Data is measured by the contact method using three different strategies for cylindricity measurement on the coordinate measurement machine (CMM) Contura G2, Carl Zeiss. For particular measurement strategies, the data is evaluated by Calypso 5.0 software (CMM) Contura G2 and Matlab/Octave software. In order to compare the collected data, we use the parameters of possible axes positions of two coaxial cylinders and their least radial distance. In the last part of this paper, there is the discussion regarding obtained parameters of evaluating methods.

1. Introduction

Fine measurement of the cylindricity is complicated and it requires 3D Coordinate Measuring Machine (CMM). CMMs are equipped with the software that allows the operator to choose measurement parameters and evaluate associated features. Obtained accuracy of the measurement and time needed for the measurement are the

important indicators, during repeated measurement in CNC regime. The choice of the measurement strategy influences economic effectiveness. The problem is how to set the strategy for the measurement of geometric features of parts and what associated integral features should be used for cylindricity evaluation. The real feature of part function is the criterion of selection of the particular associated feature when evaluating the measurement. Then, during the process of measurement strategy selection and the process of evaluation, the require-

ments for measurement accuracy become crucial. It is highly recommended to measure in a way that a particular function of the part requires. Since there are no specific standard methods for the choice of the measurement strategy, the operator of the machine plays an important role [1].

As shown in the Figure 1, EN ISO 12180-2:2011 describes four measurement strategies, i.e. measurement strategy of roundness profiles, measurement strategy of generatrix lines, measurement strategy for helix, and points measurement strategy.

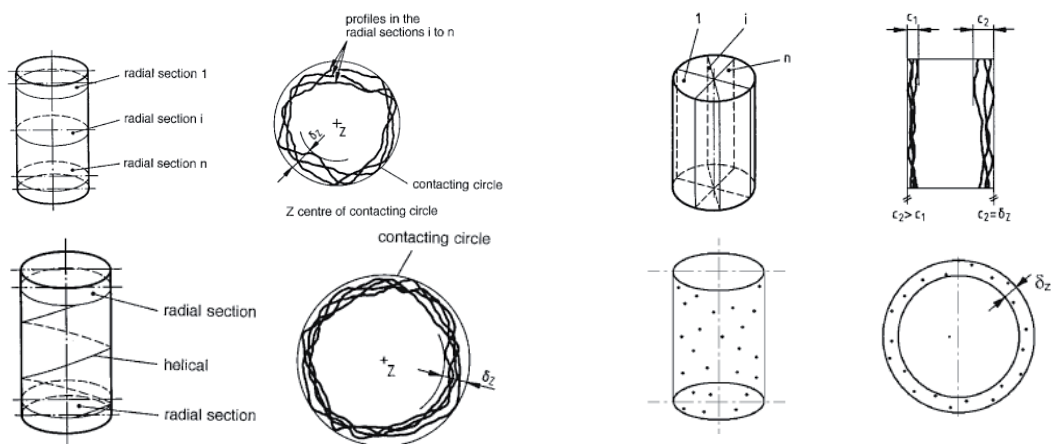


Fig. 1: Measurement strategies [2].

In metrological practice, in order to evaluate cylindricity, as shown in Figure 2, these four associated features are used: LSCY, MZCY, MICY (maximum inscribed) and MCCY (minimum circumscribed) cylinders. Each of these cylinders has its advantages and disadvantages [3, 4, 5, 6, 7, 8]. Let us present experimental results of the cylindricity deviation analysis.

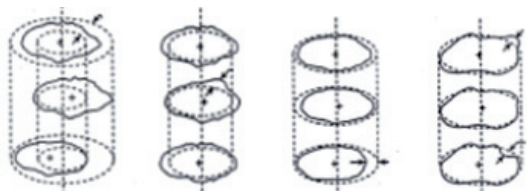


Fig. 2: An example of the associated features of cylindricity evaluation (a – MZCY, b – MICY, c – MCCY, d – LSCY).

2. Experiment

The measurement of cylindricity deviations was performed by CMM Contura G2 VAST XXT (see Figure 3) that is equipped with Calypso 5.0 software

with following parameters:

■ **Maximum permissible error (MPE) for length measurement with Contura G2 (size 7/10/6) with RDS holder and VAST XXT sensor is $MPEE = (1,8 + L/300) \mu\text{m}$, where L is measured length in mm (according to EN ISO 10360-2).**

■ **Maximum permissible scanning probing error is $MPETHP = 3,5 \mu\text{m}$ for required measuring time 68 s (according to EN STN ISO 10360-4).**

■ **Maximum permissible error for form measuring is $MPERONT = 1,8 \mu\text{m}$ (according to EN ISO 12181 and VDI/VDE 2617 part 2.2).**

Measured nominal diameter of parts equals to 20 mm. A series of measurements was performed in scanning mode with the speed of 5 mm/s. Diameter of stylus type - 3 mm, stylus length - 50 mm.

Series of parts measurement, shown in Figure 4, was realised by three measurement strategies in scanning mode (see Figure 5).

Let us describe used measurement strategies:

■ **Measurement strategy of roundness profiles – 165 measured points.**

■ *Measurement strategy of generatrix lines – 156 measured points.*

■ *Measurement strategy for helix – 179 measured points.*



Fig. 3: Coordinate measuring machine, Carl ZEISS Contura G2 RDS.



Fig. 4: Photo of measured parts.

roundness profiles (165 points) generatrix lines (156 points) helix (179 points)

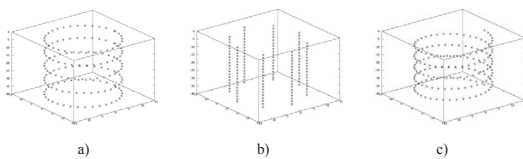


Fig. 5: Measurement strategy of parts.

4. Cylindricity Deviations Analysis

When evaluating the circularity, we used standard definition of the tolerance zone, i.e. "The tolerance zone is limited by two coaxial cylinders with a difference in radii of tolerance."

According to ISO 1101:2004, the cylindricity deviation is a difference between the largest and the smallest radial distances of the part surface from associated cylinder. The position of axes of the cylinders and values of the radii must be chosen such that the difference between two coaxial cylinders of radii equals to the smallest possible value [3].

For the analysis of the measured data, we used Octave, Matlab and Calypso 5.0 software of CMM. The analysis was performed for the data obtained by three strategies (roundness profiles (O), generatrix lines (L) and helix (H)).

Parameter calculations of associated cylinders were realised in Octave or Matlab software in three ways:

1. Parameters of cylinders with vertical axis are set using Linear Least Square method (LLS) for which the sum of squares is minimal. In this case, the problem is reduced and circularity deviations are set by the coordinates of x and y. This method is described in more details in [9].

2. The solution of this problem using LLS has been used as an initial approximation for determination of two perpendicular coaxial cylinders with the condition of minimum zone (ICMZ). Of course, this problem solving gives minimum deviation from cylindricity using LLS method.

3. Furthermore, the ICMZ serves as an initial approximation for the solution of coaxial cylinders with minimum zone (CMZ), this time from the tilted axis of symmetry. This problem was solved by the following function Octave and/or Matlab.

```
fminsearch('width_cylinder';x0,opt),
```

where the unknown are the coordinates of points x and y intersecting the axis with the plane $z = z_{\min}$ and $z = z_{\max}$. These points are recorded in Table 1 as lower and upper centre. The cylindricity deviation obtained in this way, using CMZ method, is undoubtedly smaller than two above mentioned values computed for LLS and ICMZ methods.

Time is an important factor when using LLS, ICMZ and CMZ for computer calculations compared to the measurement itself. Therefore, we may suppose that the most accurate results are the results that provide the most complete information about a part, e.g. results of data processing for all 500 measured data. In the table, these results are denoted as SUM.

Calculated parameters using Octave and/or Matlab software are presented in Table 1.

5. Conclusion

The comparison of three different measurement strategies was performed using the cylindricity deviation. CMM Contura G2 is equipped with Calypso 5.0 software. Data analysis focused on the strategies of measurement. Outcome data from the programme are not sufficient for such analysis. In order

Table 1: Calculated parameters.

	Characteristics		LLS	ICMZ	CMZ	Calypso
O	Position of the lower centre	x_c [mm]	-0.008245	-0.006368	-0.015885	6.7
		y_c [mm]	0.012186	0.013656	0.025135	
	Position of the upper centre	x_c [mm]			-0.001942	
		y_c [mm]			-0.000771	
	Deviation angle from vertical axis	[degree]	0	0	0.048	
L	Outer radius	r [mm]	11.500270	11.500023	11.487044	9.5
	Cylindricity deviation	Δr [μ m]	32.876	31.909	6.786	
	Position of the lower centre	x_c [mm]	-0.008347	-0.008347	-0.015885	
		y_c [mm]	0.013076	0.013076	0.025135	
	Position of the upper centre	x_c [mm]			-0.018173	
H		y_c [mm]			0.026569	6.7
	Deviation angle from vertical axis	[degree]	0	0	0.054	
	Outer radius	r [mm]	11.500583	11.499520	11.488441	
	Cylindricity deviation	Δr [μ m]	31.630	29.827	9.770	
	Position of the lower centre	x_c [mm]	-0.007318	-0.005262	-0.015063	
SUM		y_c [mm]	0.012093	0.012248	0.025552	6.7
	Position of the upper centre	x_c [mm]			-0.018173	
		y_c [mm]			0.026569	
	Deviation angle from vertical axis	[degree]	0	0	0.049	
	Outer radius	r [mm]	11.500733	11.499564	11.487635	
SUM	Cylindricity deviation	Δr [μ m]	29.501	28.426	8.024	6.7
	Position of the lower centre	x_c [mm]	-0.007944	-0.005917	-0.016914	
		y_c [mm]	0.012427	0.013165	0.026481	
	Position of the upper centre	x_c [mm]			-0.018173	
		y_c [mm]			0.026569	
SUM	Deviation angle from vertical axis	[degree]	0	0	0.049	6.7
	Outer radius	r [mm]	11.501385	11.500688	11.488928	
	Cylindricity deviation	Δr [μ m]	33.872	33.193	10.164	

to compare the expedience and the efficiency of the measurement strategy, more information on quantitative indicators is necessary, e.g. measurement accuracy, time of measurement, part function, etc. This information can be obtained during further data processing. In this paper, we used Octave and Matlab software that produce more detailed information from the data obtained by the measurement.

Our results are presented in Table 1. The data was obtained by the tactile probe. Recommended speed of scanning and other requirements are set by the good practice measurement [1]. Despite these facts, we cannot definitely recommend either the expedience of used measurement strategy or the expedience of use of associated feature for cylindricity deviation evaluation.

Further research should focus on the solution of the influence of other factors that may bias the results of measurement. It may lead to a proposal of the classification of measurement principles defined in standards.

6. Acknowledgements

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