

Experimental Verification of Abrasive Mass Flow Impact on the Technological Head Acceleration Amplitude and Vibrations Frequency in the Production System With AWJ Technology

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KEY WORDS

Experiment, material cutting, hydroabrasive water jet, cutting parameters, abrasive, abrasive mass flow, vibration, frequency, amplitude.

ABSTRACT

Between the technological parameters that influence the acceleration amplitude and vibrations frequency on technological head in the production system (PS) with water jet technology belongs the abrasive mass flow. The article is focused on examination of the ukrainian garnet abrasive mass flow on technological head vibrations and their frequency spectrums during cutting material HARDOX 500. The article includes description of experiment and measurement results carried out in laboratory workplace with water jet technology.

1. Introduction

During the operation of manufacturing systems with hydroabrasive jet technology, arising in the production system vibrations, which affect its reliability and durability, operating costs and consequently economic efficiency and operational safety. The emergence and spread of vibrations generated by water jet technology remains actual and theoretically difficult issue, which is currently not sufficiently developed. Despite the best efforts of researchers and a good knowledge of the operation in PS with water jet technology remains unexplained facts. One of them is the abrasive mass flow technological parameter affecting the acceleration amplitude and vibrations frequency on technological head, which is the subject of experimental investigation during cutting steel HARDOX 500.

2. Experimental Sections

The experiments were conducted in liquid jet laboratory IF HGF VŠB TU in Ostrava. The main parameters of PS with AWJ technology: [4]

■ *multiplicator.*

The high pressured pump PTV 19/60 on the basis of the pump Flow HSQ 5X (the pressure up to 415 MPa, the passage up to 1,9 l.min⁻¹)

■ *the working area of the vat.*

X-Y CNC table WJ1020-1Z-EKO with the accessories

■ **technological head Paser IIITM.**

The type of the nozzle 10, the length of the abrasive nozzle 76 mm.

Conditions of experiment

Table 1 shows the factors and conditions under which the experiment was realized.

Table 1: Overview of experimental conditions

Material factors	divided material	steel K13 – HARDOX 500
	material thickness	10 mm
Technological factors	pressure	380 MPa
	cutting speed	100 mm.min ⁻¹
	type of abrasives	Ukrainian garnet
Factors abrasives	abrasive grain size	MESH 80
	abrasive mass flow	100 g.min ⁻¹
		300 g.min ⁻¹
		500 g.min ⁻¹
		700 g.min ⁻¹
Mixing factors	the diameter of the water nozzle	0,25 mm
	the diameter of the directing tube	1,02 mm

All measurements were made from the same starting position X = 320 mm, Y = 370 mm.

3. Hardware and Software for Data Processing

Hardware: The piezoelectric accelerometer from the Brüel & Kjær (type: 4507-B-004, parameters: IEPE, TEDS, 1-axial, 100mV/g) was mounted to the head so that its axis was identical to the vibrations axis in the direction of the abrasive water jet. The accelerometer was connected to the AD converter (AI ±5V IEPE, sampling 25kSps) through which was created the data record, stored in the PC as a time record of the vibration acceleration signal.

Software: For the time signal evaluation was used SignalExpress software, which is a part of the programming and development environment of LabVIEW from National Instruments. From the time record a steady part during 10 seconds was selected

and by using the Fourier transformation a frequency spectrum in the range from 0 to 10 000 Hz was generated. By using a filter (algorithm) we received an envelope of frequency spectrum. [3]

4. Measured and Graphically Preprocessed Values

The measured values are processed in the frequency spectrum range from 0 to 10 kHz and are presented in graphical form broken down for individual feed rates of technological head. On Figs. 1, 3, 5 and 7 are evaluated the frequency spectrums of vibration acceleration amplitudes for the used abrasive mass flows of 100, 300, 500 and 700 g.min⁻¹. On Fig. 2, 4, 6 and 8 are shown graphically the envelopes of frequency spectrums vibration amplitudes of the technological head for the used abrasive mass flows. [4]

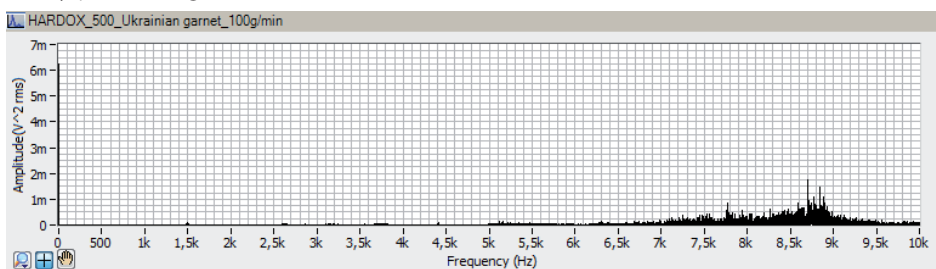


Fig. 1: The vibrations spectrum on the technological head for the mass flow $m_a = 100 \text{ g.min}^{-1}$

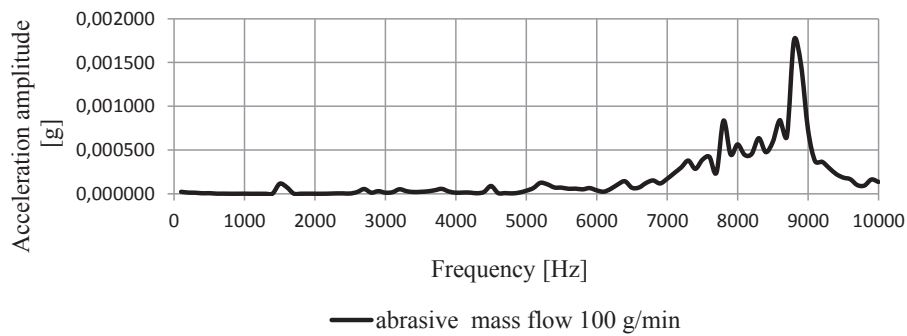


Fig. 2: The envelope of vibrations frequency spectrum on the water jet technological head for the mass flow 100 g.min⁻¹.

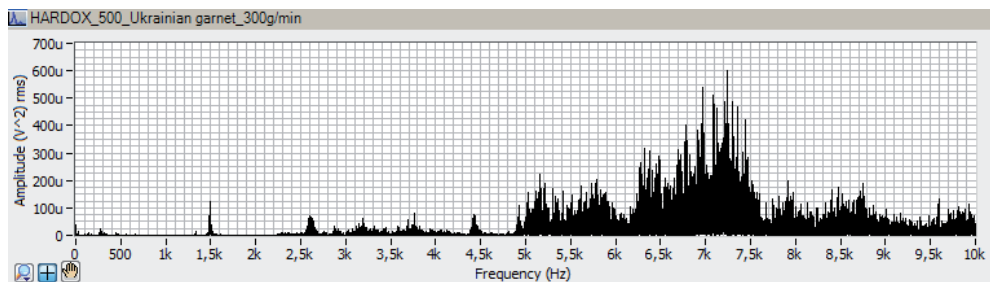


Fig. 3: The vibrations spectrum on the technological head for the mass flow $m_a = 300 \text{ g.min}^{-1}$.

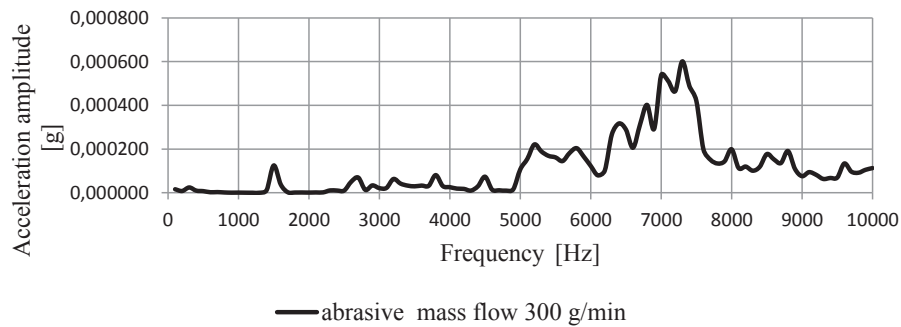


Fig. 4: The envelope of vibrations frequency spectrum on the water jet technological head for the mass flow 300 g.min⁻¹.

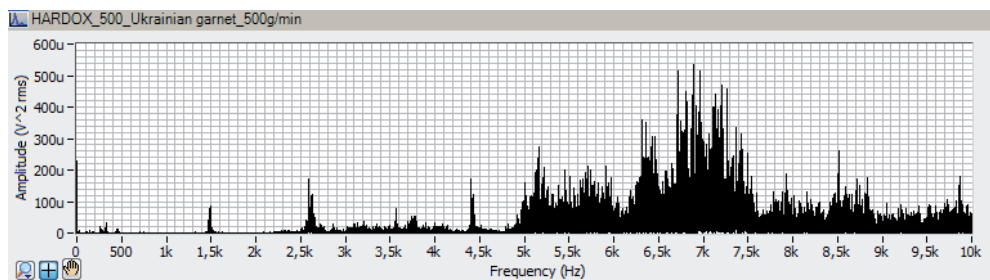


Fig. 5: The vibrations spectrum on the technological head for the mass flow $m_a = 500 \text{ g.min}^{-1}$.

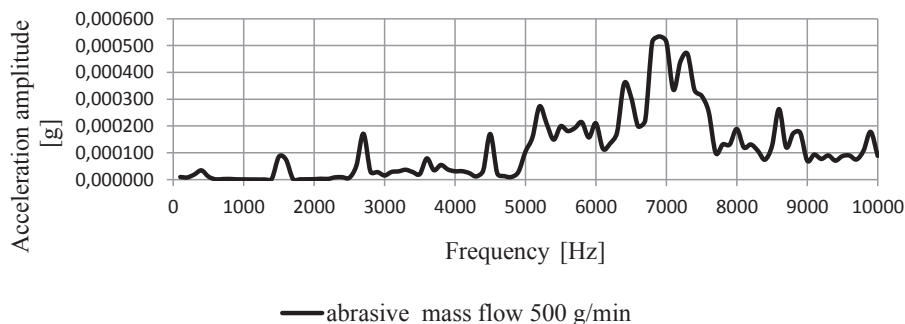


Fig. 6: The envelope of vibrations frequency spectrum on the water jet technological head for the mass flow 500 g.min⁻¹.

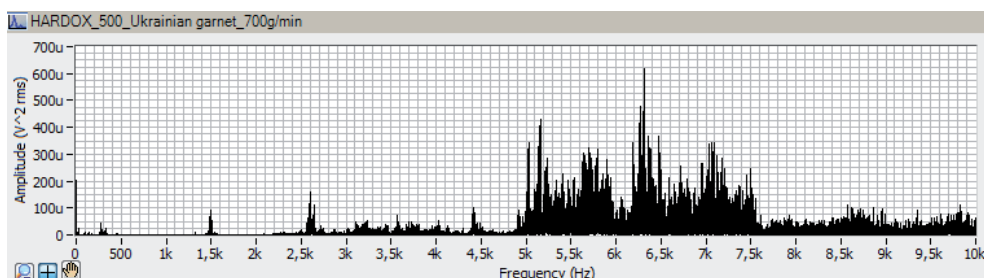


Fig. 7: The vibrations spectrum on the technological head for the mass flow $m_a = 700 \text{ g.min}^{-1}$

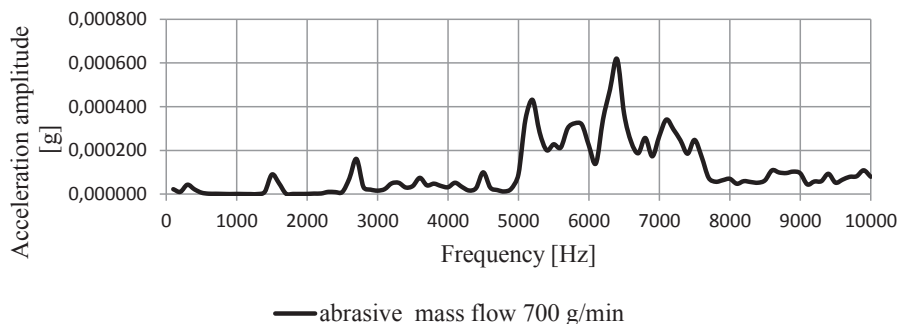


Fig. 8: The envelope of vibrations frequency spectrum on the water jet technological head for the mass flow 700 g.min⁻¹

5. New Knowledge Obtained by Evaluating of Experiments

From the group of ukrainian garnet abrasive mass flows in the experiment when dividing steel HARDOX 500 with MESH 80 grit it were found the smallest vibrations values for the abrasive mass flow 500 g.min⁻¹ where were the maximum vibration acceleration amplitude measured of 0,534 mg at a frequency of 6,9 kHz. When using the mass flows of 100 g.min⁻¹, 300 g.min⁻¹ and 700 g.min⁻¹ occurred during cutting one increased band of vibrations acceleration amplitude for each investigated mass

flow. The increased band of mass flow 700 g.min⁻¹ occurred in the frequency range from 5,0 to 7,5 kHz where the maximum vibrations acceleration amplitude reached a value of 0,618 mg at a frequency of 6,4 kHz. One band of vibration acceleration amplitude occurred when using mass flow 300 g.min⁻¹ in the frequency range from 6,2 to 7,7 kHz, where was the maximum vibrations acceleration amplitude measured 0,601 mg at a frequency of 7,3 kHz. Less favorable vibrations amplitudes from the evaluated set of mass flows were measured at a flow of 100 g.min⁻¹, where the increased band occurred in the

frequency range from 7,0 to 9,5 kHz with maximum vibrations acceleration amplitude of 1,751 mg at a frequency of 8,8 kHz. In all the abrasive mass flows used during cutting in the frequency range from 5,0 to 7,5 kHz are found approximately the same acceleration amplitude values ranging from 0,107 mg to 0,42 mg.

6. Conclusion

From the experiment evaluation is clear, that the abrasive mass flow has, but in the difference scale on the formation, spread and intensity of technological head vibrations in the water jet cutting process. Based on the graphical dependencies review from the vibrations process can be said, that when cutting steel HARDOX 500 of thickness 10 mm, feed rate 100 mm.min⁻¹ and a pressure of 380 MPa in terms of vibrations is preferable to use the abrasive mass flow of 500 g.min⁻¹ in comparison with the mass flows of 100 g.min⁻¹, 300 g.min⁻¹ a 700 g.min⁻¹. Even when the vibrations acceleration amplitude value reached in the experiment in the worst case value 1,751 mg at a frequency of 8,8 kHz the value in operation for prolonged exposure although may have some negative impact on reliability, durability, operating costs, economic efficiency and operation safe of the PS with AWJ technology. However, this adverse effect does not reach significant adverse up to critical values.

7. References

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